

Internal Stresses in Tungsten Fiber Reinforced Bulk Metallic Glass Matrix Composites

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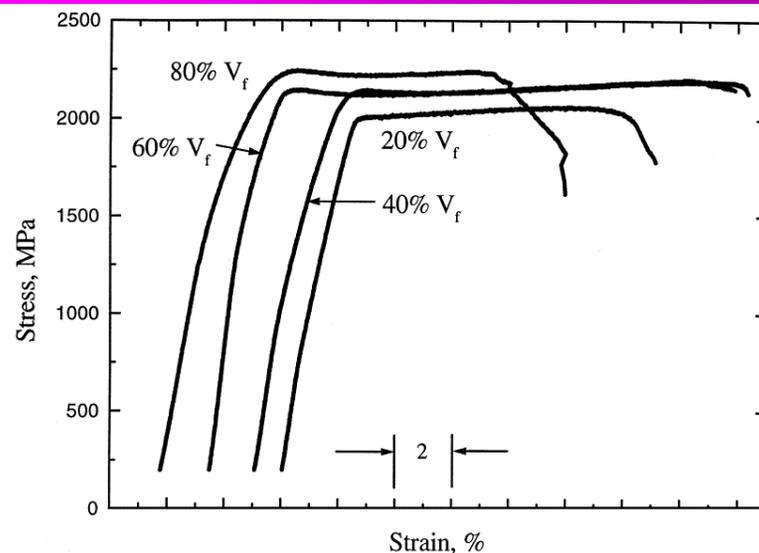
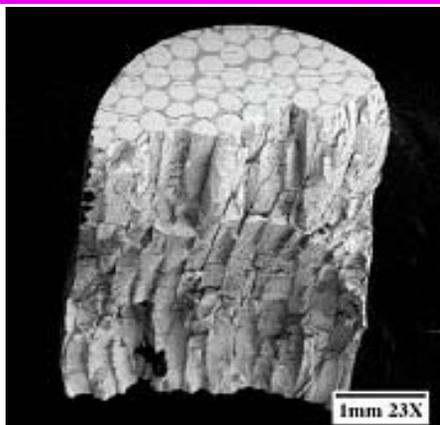
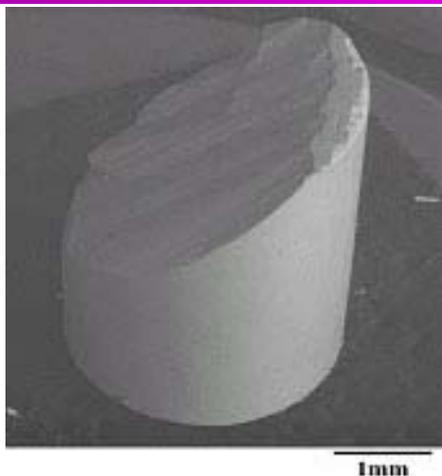


Outline

- BMG matrix tungsten fiber composites
- Neutron diffraction
- Finite element modeling
- Results
- Conclusion

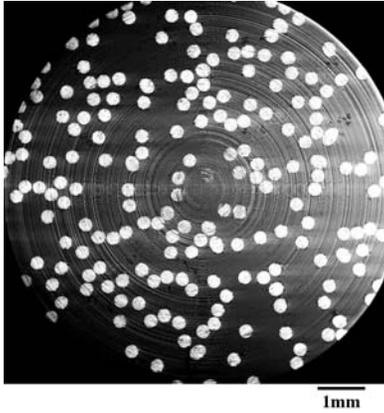


BMG matrix tungsten fiber composites

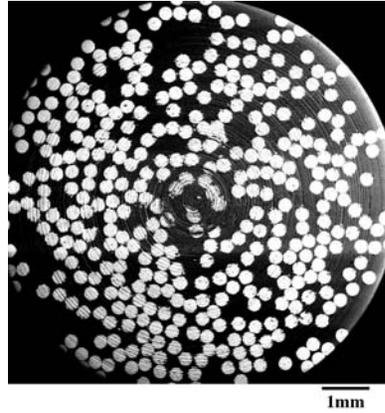


- Vit1: $Zr_{41.2} Ti_{13.8} Cu_{12.5} Ni_{10} Be_{22.5}$
- BMG/Tungsten fiber composites
 - Same ultimate stress as monolithic Vit1
 - Large increase in ductility
 - Knee in stress strain curve as tungsten fibers yield

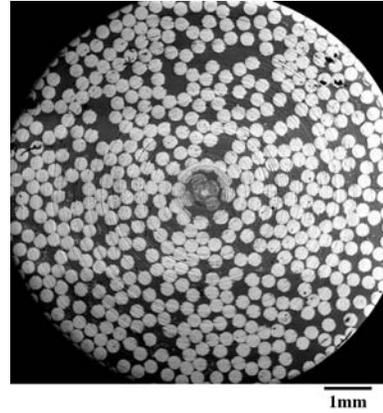
BMG matrix tungsten fiber composites



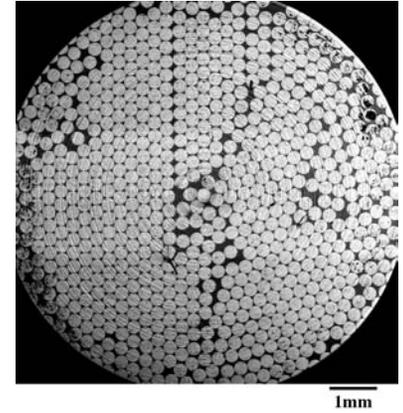
20% (21.0%)



40% (42.4%)



60% (61.9%)

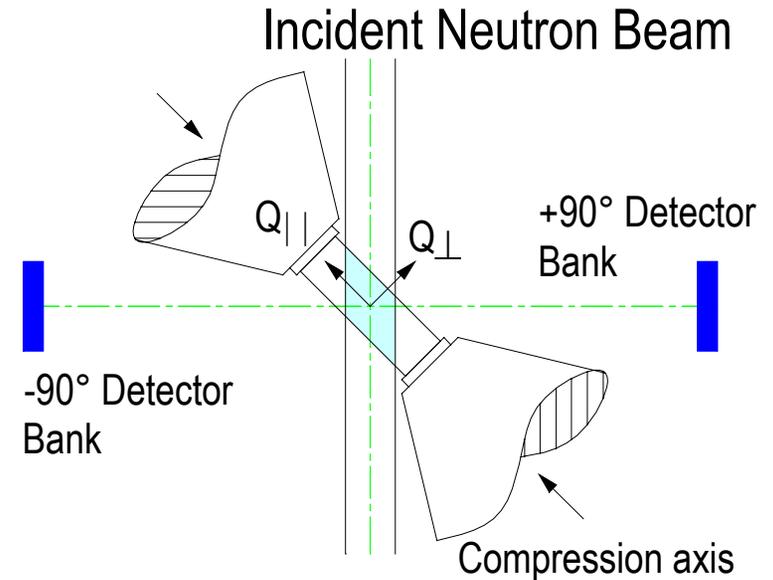


80% (84.2%)

- Measured volume fractions deviates slightly compared to nominal volume fractions
- “Agglomeration” seen for all volume fractions
- “Stacking faults” seen for the 80% sample



Neutron diffraction



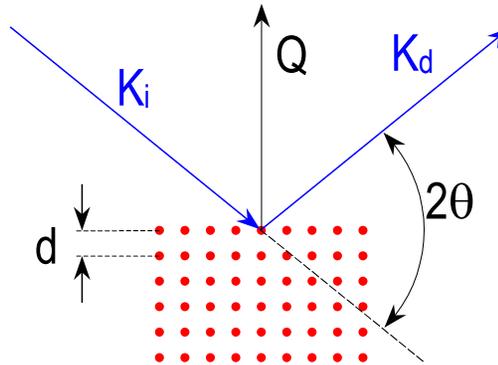
- Spectrometer for **M**aterials **R**esearch at **T**emperature and **S**tress (**SMARTS**)
- Schematic set-up for *in-situ* compression loading
- Measurement time is about 10-20 minutes per load level
- Measure elastic strains in two directions simultaneously
- Bulk measurement contrary to conventional X-ray measurements



Neutron diffraction

$$\lambda = 2d\sin\theta$$

- Fixed λ ; Reactor (steady state). Measure intensity as function of angle
- Fixed θ : TOF (spallation). Measure intensity as function of time-of-flight

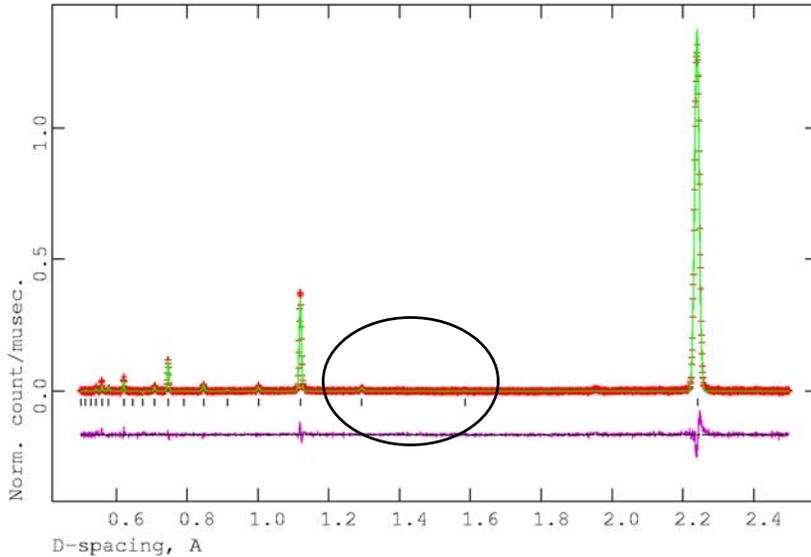


- Differences in lattice spacing => **Only Elastic Lattice Strain of Crystalline Phase**

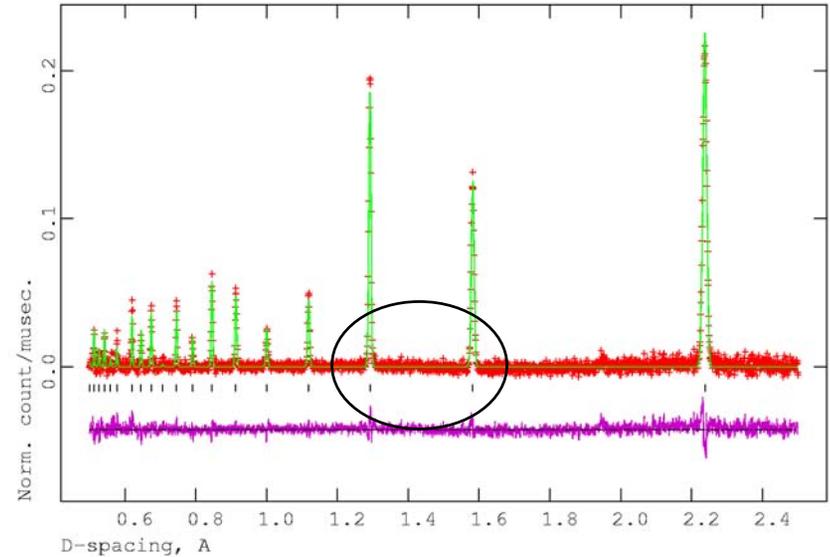
$$\varepsilon_{hkl}^{el} = \frac{d_{hkl} - d_{hkl}^0}{d_{hkl}^0} = \frac{d_{hkl}}{d_{hkl}^0} - 1$$



Neutron diffraction



Parallel



Perpendicular

- Diffraction patterns from BMG tungsten fiber composite sample (80%)
- Highly textured fibers; hh0 texture for wire drawn bcc metals
- Good statistics from short count times
 - $R_{wp} \approx 6-8\%$, strain error bar $\approx 15 \mu\epsilon$



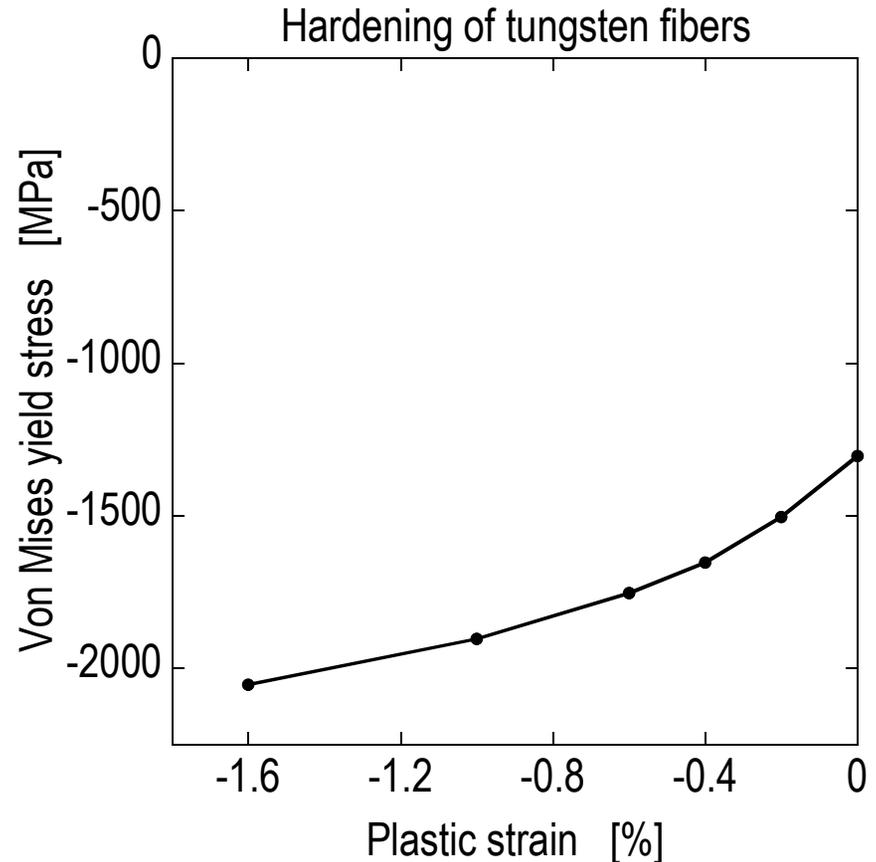
Finite element model input

- BMG

- Young's modulus: 96 GPa
- Poisson's ratio: 0.36
- Yield stress (Mohr-Coulomb):
 $\tau_c = 946 - 0.04\sigma_n$ [MPa]
- No hardening

- Tungsten

- Young's modulus: 410 GPa
- Poisson's ratio: 0.28
- Yield stress (Von Mises):
 $\sigma_y = 1305$ [MPa]
- Hardening as shown in plot



R. D. Conner, R. B. Dandliker and W. L. Johnson, *Acta Mater.*, vol. 46(17), pp. 6089-6102, 1998

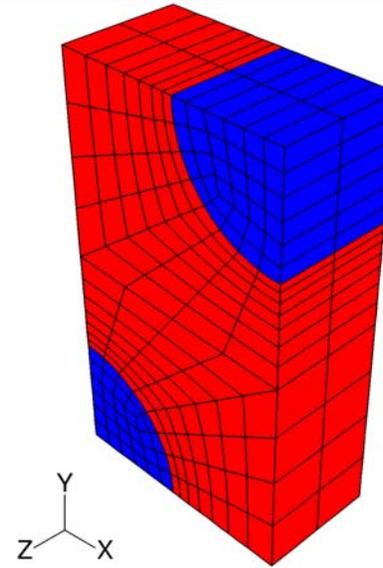
Lewandowski J. J. and Lowhaphandu P., *Phil. Mag. A.*, in print

A. Saigal and G.G. Leisk, *Mat. Sci & Eng. A*, vol. 237, pp. 65-71, 1997

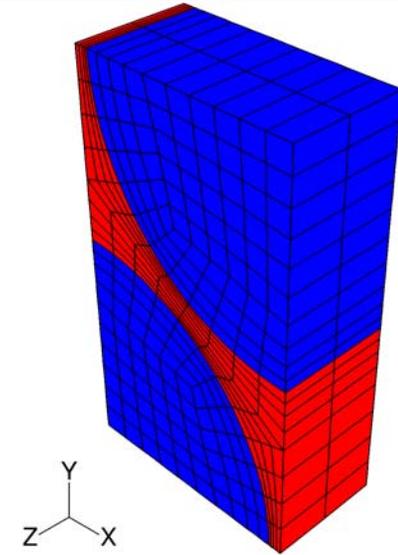


Finite element model

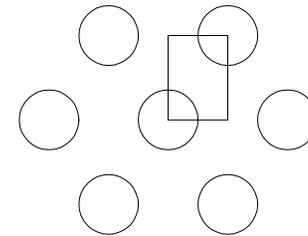
- Full 3D model due to loading along fibers
 - Unit cell model
 - Plane strain by keeping planes perpendicular to fibers plane
 - Brick 2nd order elements
- Hexagonal stacking in all models to accommodate high volume fractions
- Thermal cooling cycle
 - Same ΔT as previously found to give good comparison with measured thermal residual stresses (same for all volume fractions)



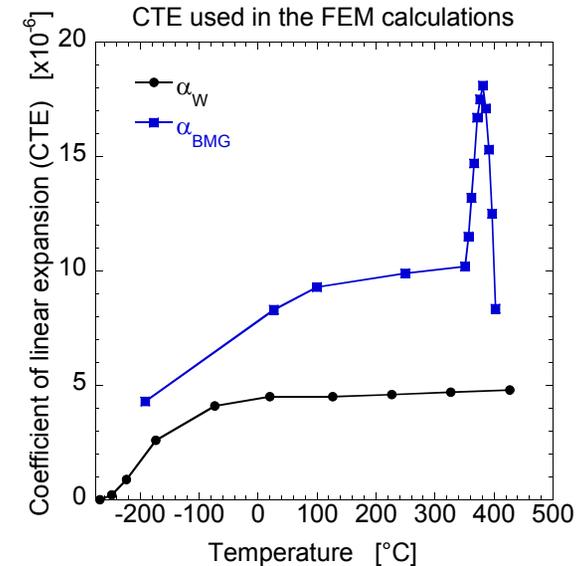
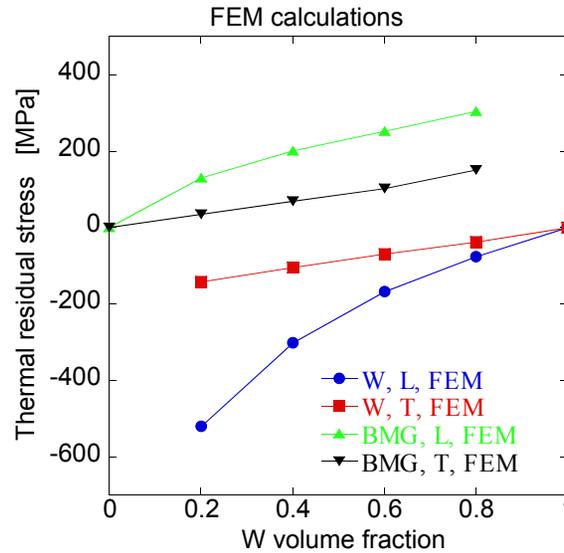
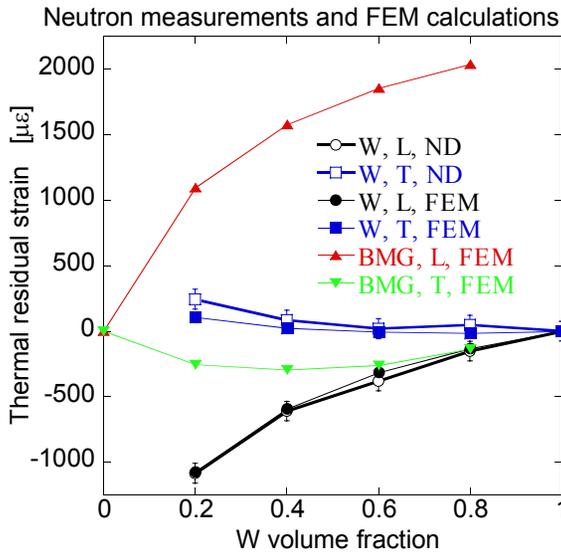
20% Mesh



80% Mesh



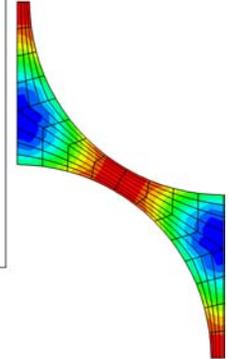
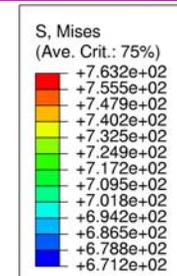
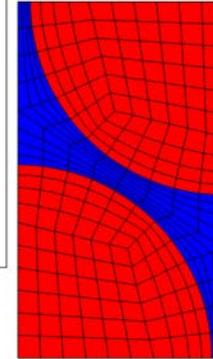
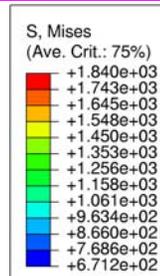
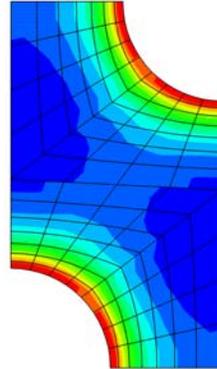
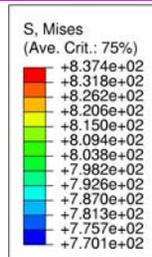
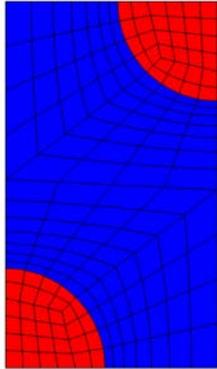
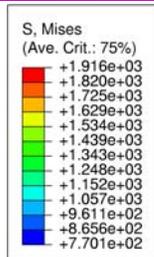
Thermal residual strains



- Measured and calculated thermal residual stresses
 - Pure elasticity
 - Good agreement for the tungsten fibers
- Predict thermal residual *stresses* in both phases



Finite element model



20% Von Mises

20% Von Mises
Matrix only

80% Von Mises

80% Von Mises
Matrix only

- Von Mises stresses at highest load level (1000MPa for 20, 1600MPa for 80%)
 - Stress concentration for the 80% - precursor for shear band formation
 - No appreciable variation of Von Mises stress in fibers

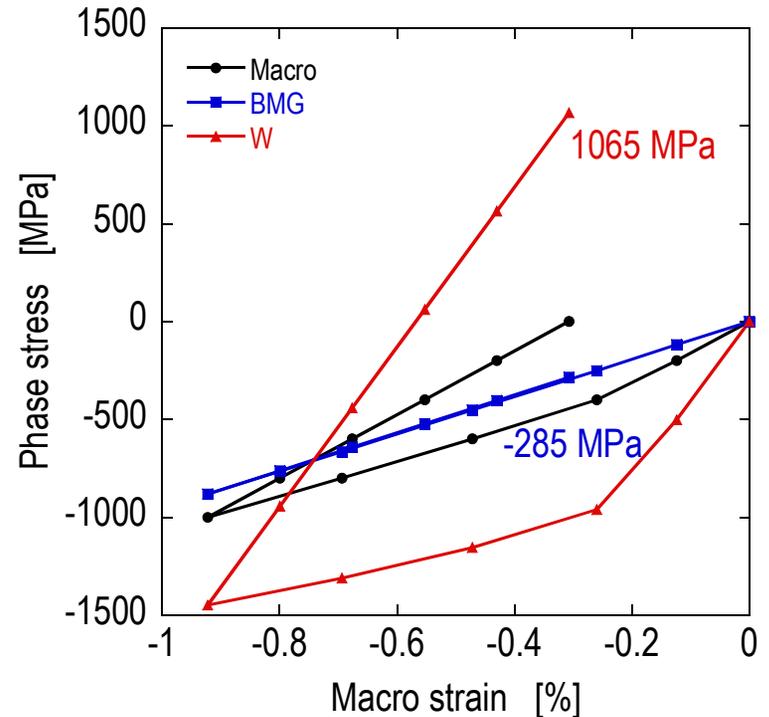
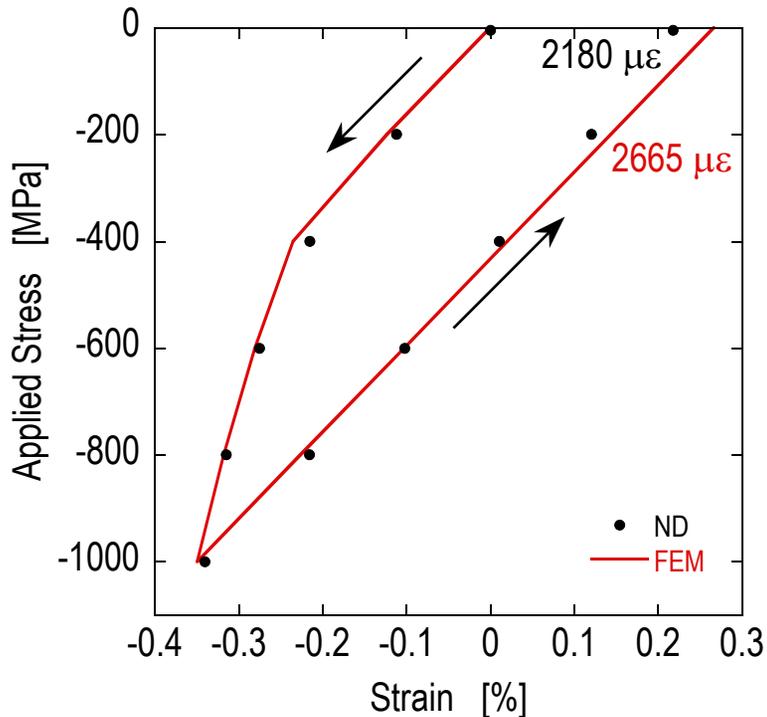


Measured lattice strains and predicted stresses, 20% sample

ND and FEM for W fiber



FEM, Load partitioning



- Good agreement with loading data; Residual strain is overestimated
- Calculated loading and unloading slopes are slightly shallower than the measured slopes

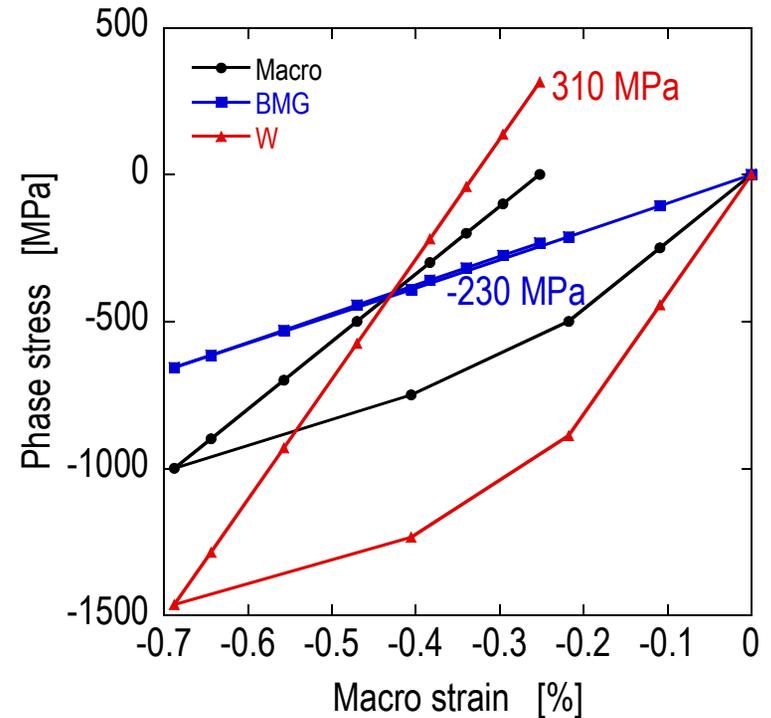
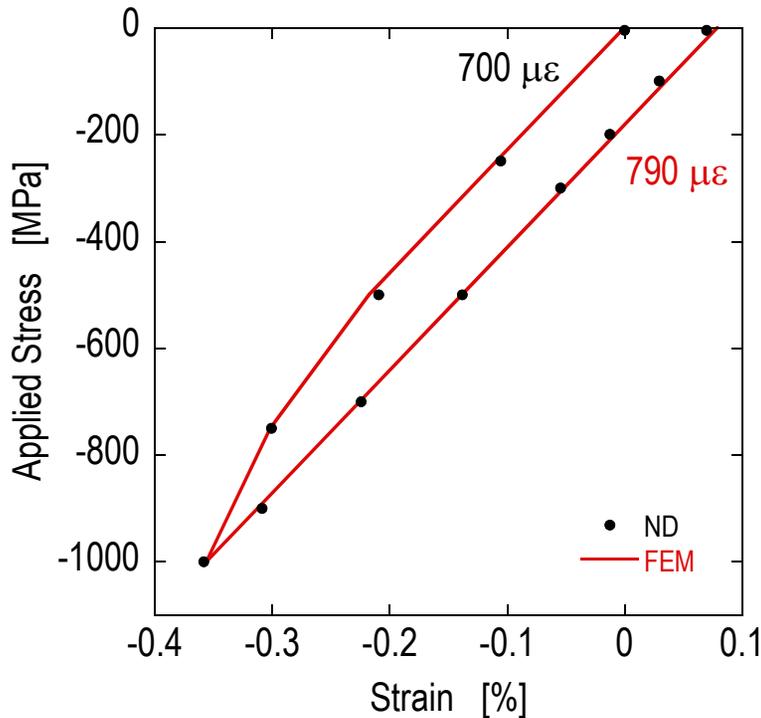


Measured lattice strains and predicted stresses, 40% sample

ND and FEM for W fiber



FEM, Load partitioning



- Good agreement with loading data; Reasonable agreement with residual data
- Good agreement with measured slopes

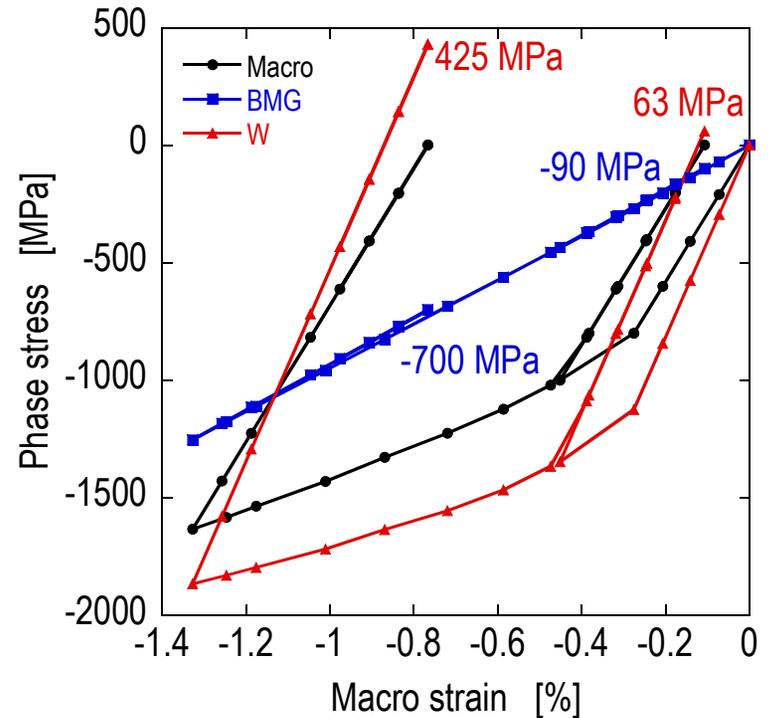
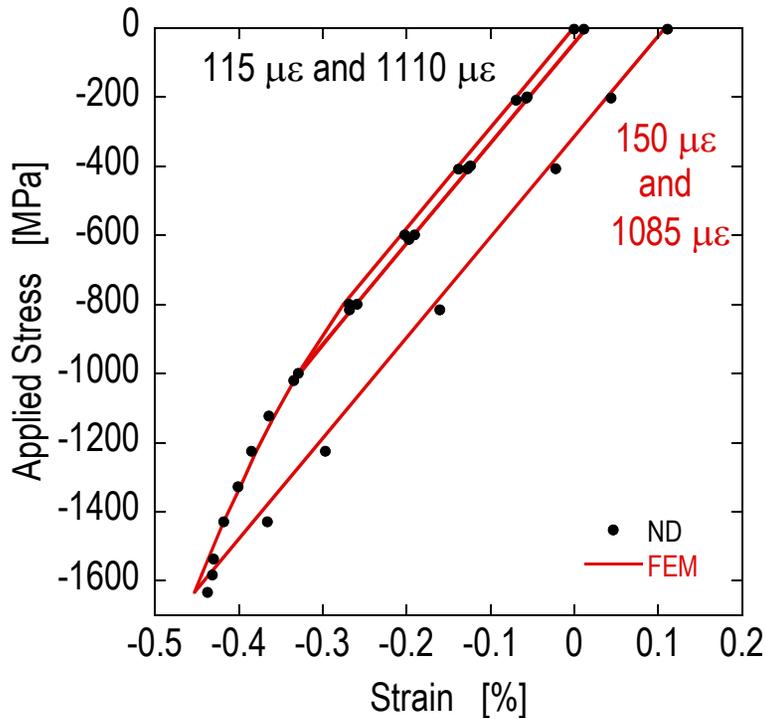


Measured lattice strains and predicted stresses, 60% sample

ND and FEM for W fiber



FEM, Load partitioning



- Overestimates strains at high load; Good agreement for residual data
- Good agreement with measured slopes

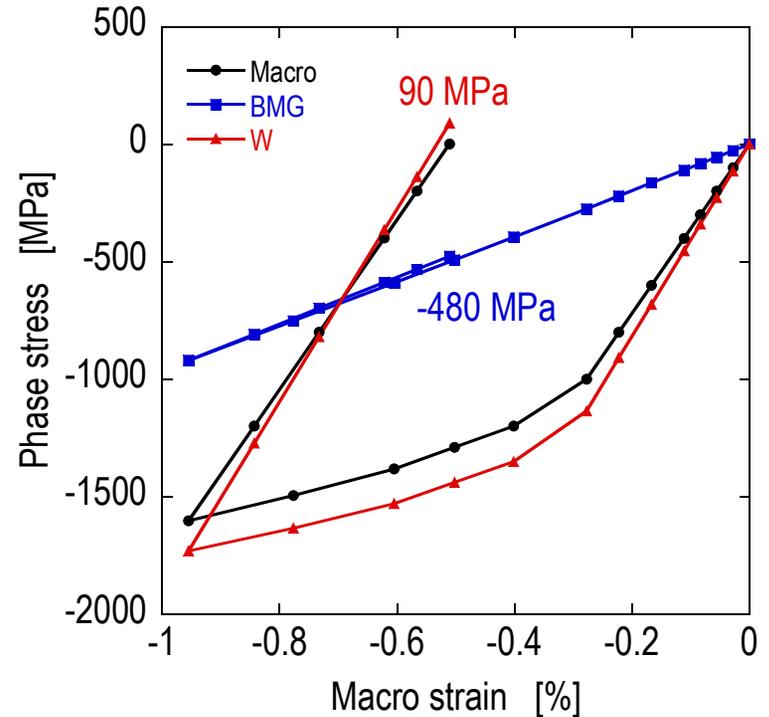
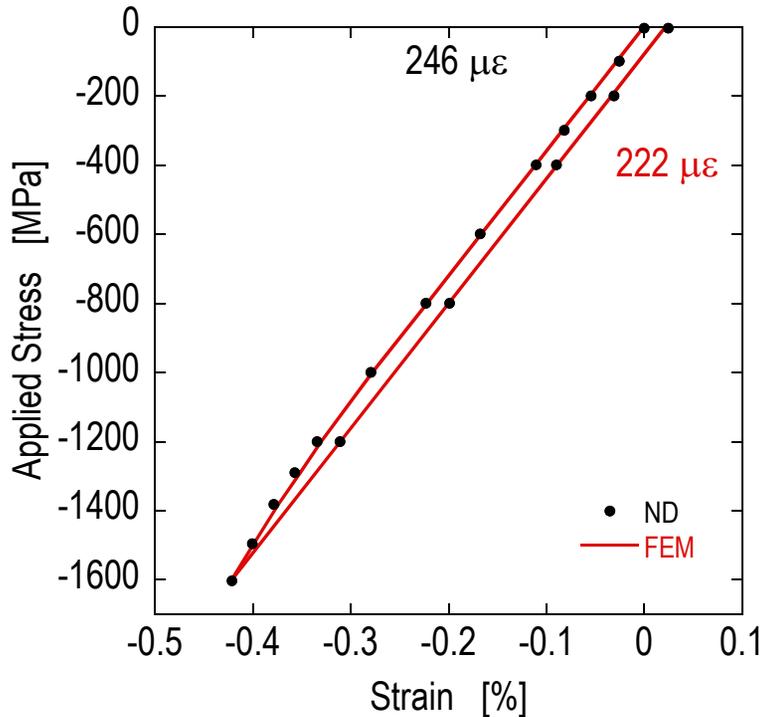


Measured lattice strains and predicted stresses, 80% sample

ND and FEM for W fiber

⇒

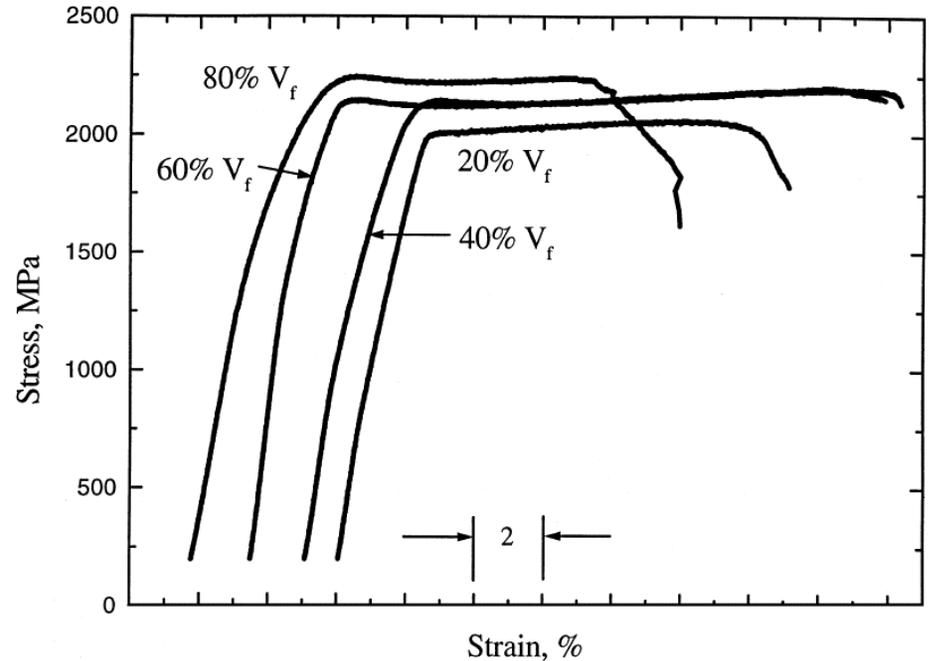
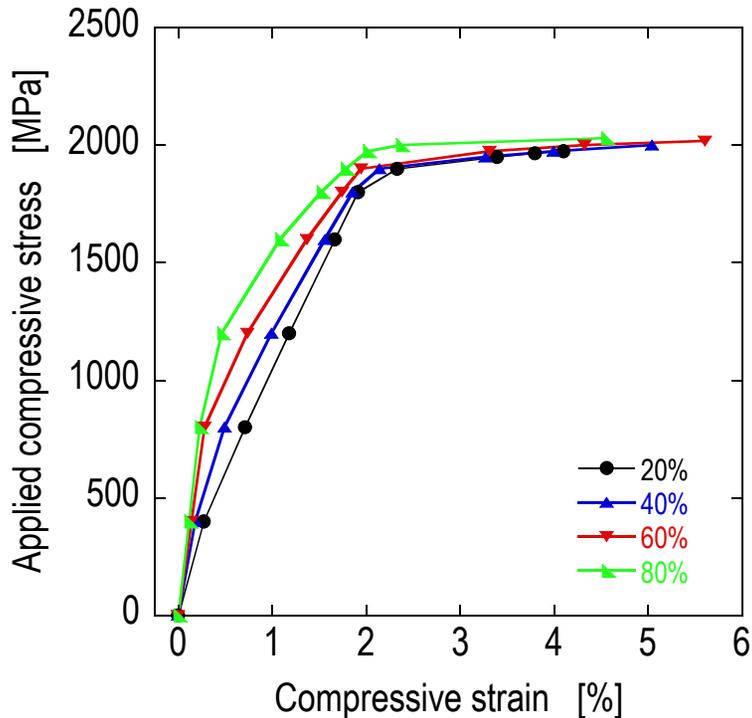
FEM, Load partitioning



- Good agreement with both loading and residual data
- Good agreement with measured slopes



Yielding in BMG



- Predicted yield stress in the BMG using Mohr-Coulomb yield criteria
 - All samples predicted to have about the same ultimate stress
- Measured ultimate stress varies as a function of fiber volume fraction

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R. D. Conner, R. B. Dandliker and W. L. Johnson, Acta Mater., vol. 46(17), pp. 6089-6102, 1998



Conclusions

- Neutron diffraction
 - 10-20 minutes count times gives adequate statistics
- Finite element modeling
 - Predictions of elastic strains in the tungsten fibers are in good agreement with the diffraction data
 - ⇒ FEM provides phase stresses, residual stresses and load partitioning
 - The Von Mises yield stress used in FEM is the same for all volume fractions and there is good agreement with the onset of non-linearity in the diffraction data for all volume fractions
 - ⇒ In-situ Von Mises yield stress of fibers seems to be unaffected by volume fraction

